

Stray Light Correction Algorithm for Multi-channel Spectrographs

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NIST

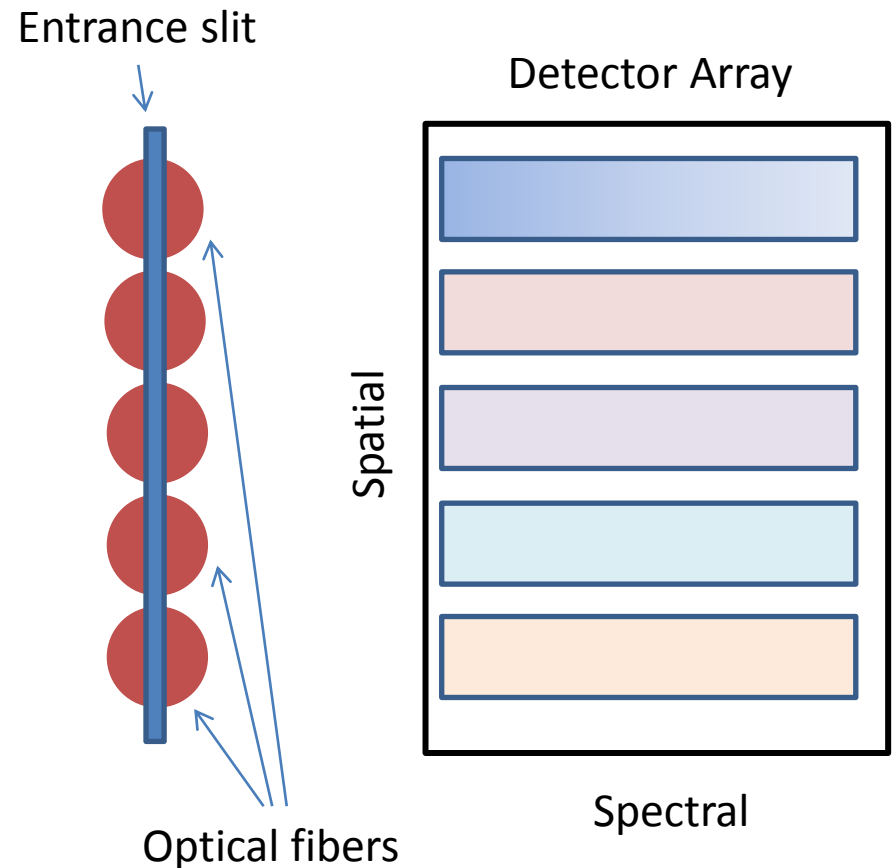
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Moss Landing Marine Laboratories

Dennis K. Clark
Marine Optical Consulting

Multi-channel Spectrographs

Typical Layout

- In a conventional single-channel spectrograph, the entrance slit is imaged on the detector plane
- In a multi-channel spectrograph, the entrance slit is divided into channels for inputs from different targets
 - Simplest way to do this is to use optical fibers – often simply epoxied onto the entrance slit



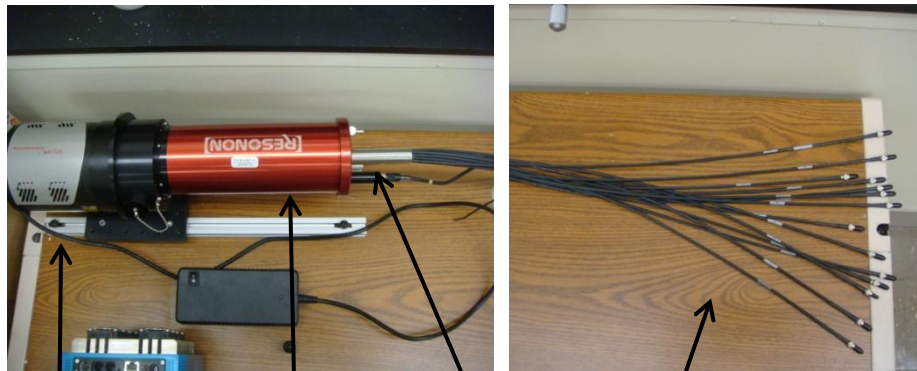
Motivation for the work arises from survey of fields with applications using Multiple-input (or multi-channel) Spectrographs

- Medical imaging
 - High throughput screening
- Machine vision
 - Multi-channel process monitoring
- Remote sensing
- Astronomy

Intermediate step between 1-d SLC algorithm and full point spread response correction algorithm

Ocean Color Multi-channel Spectrograph built by Resonon for Moss Landing

14-channel spectrograph

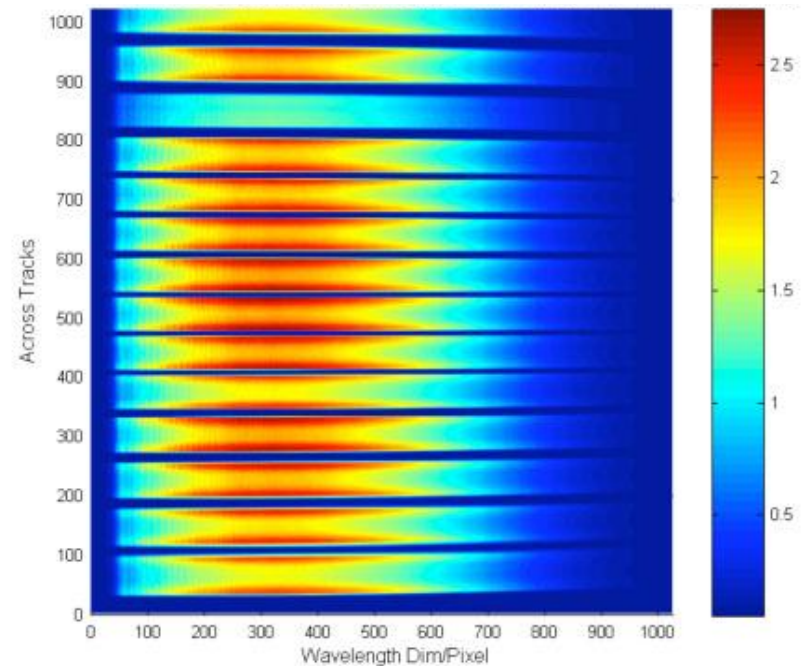


Detector

Spectrograph

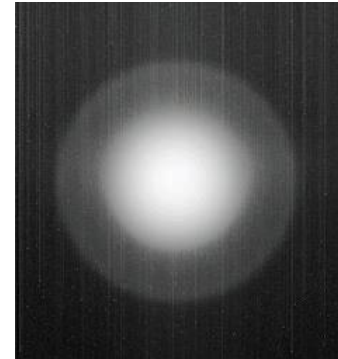
Fiber Input

Image on the CCD from an
14-channel spectrograph



Characterization/Performance Issues

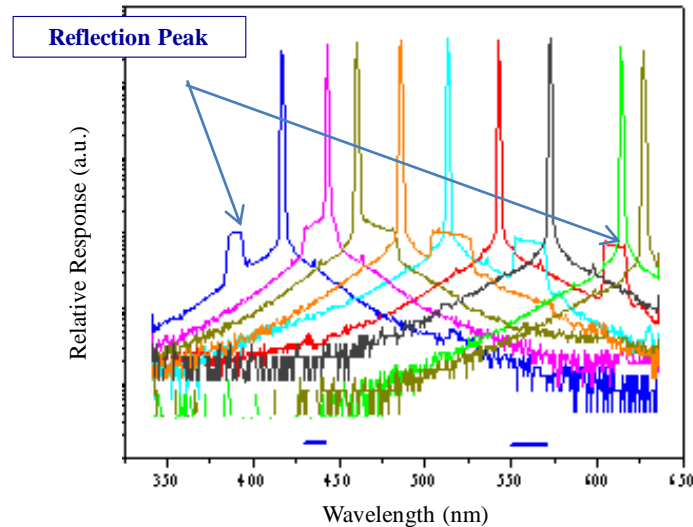
Output from a standard fiber shows an extended halo that may cause scattered light within the spectrograph



Grating scatter

Ghost image

Spurious reflection peaks

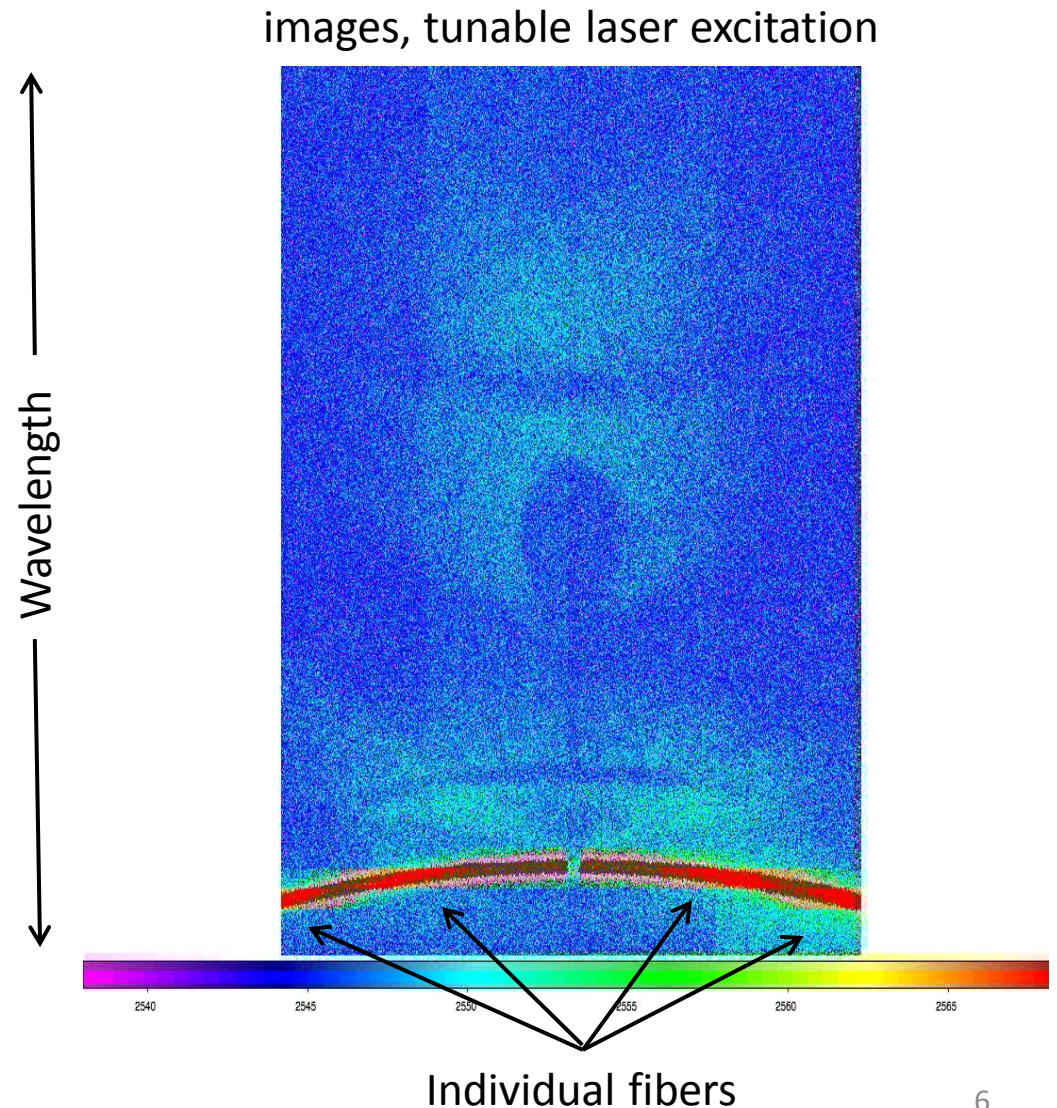


Impacts Along-track (spectral) and Cross-track (spatial) performance

Astronomy Example: Baryon Oscillation Spectroscopic Survey (BOSS)

Movie Provided by
Claire Cramer, NIST

- BOSS has 1000 fiber inputs > “Big Boss” – 5000 inputs
- 2.5 m telescope at Apache Point Observatory, New Mexico
- Used to study large-scale structure of the universe



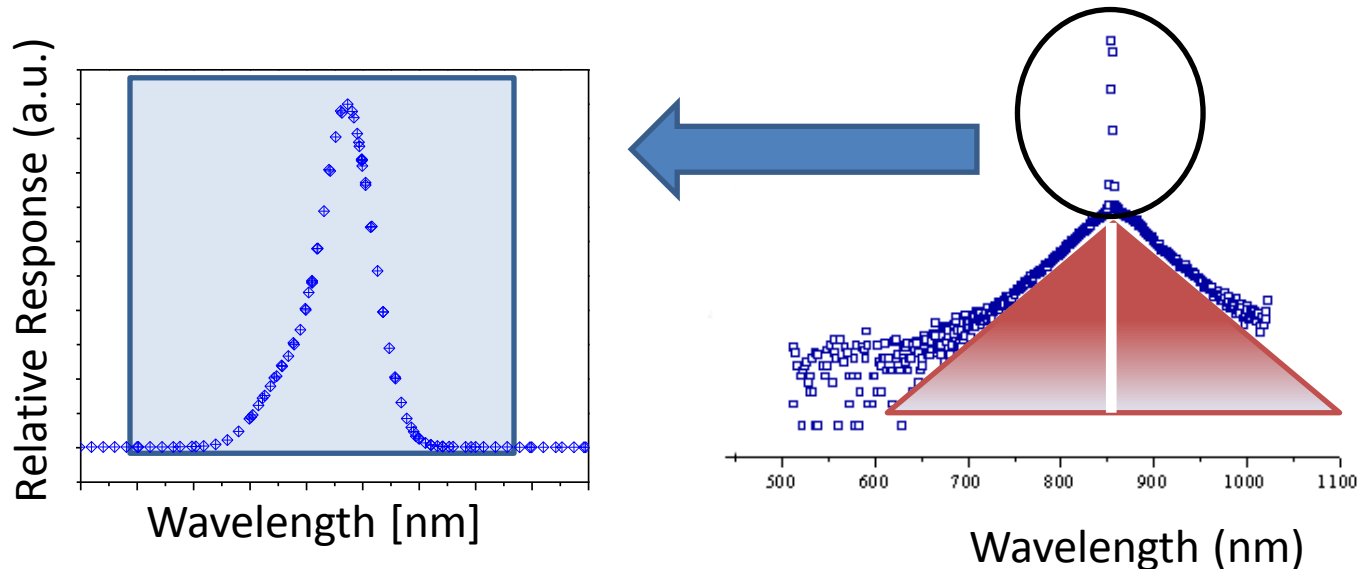
Algorithm for Single Input System: Review

$$S_{meas} = \int_{\lambda} r(\lambda) L(\lambda) d\lambda$$

In-Band

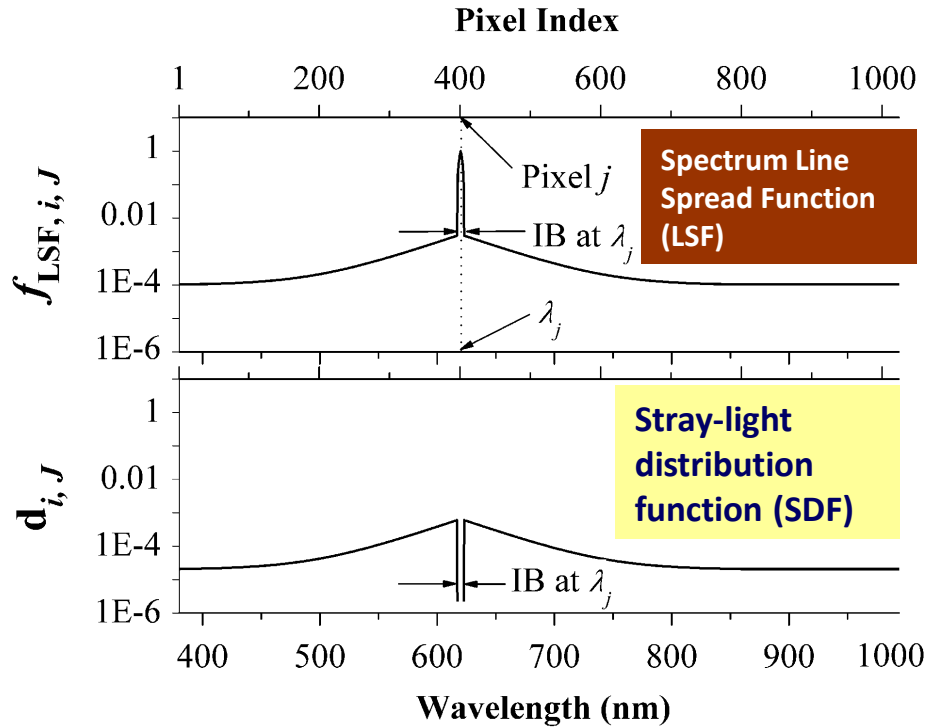
Out-of-Band

$$S_{meas} = \int_{ib} r(\lambda) L(\lambda) d\lambda + \int_{oob} r(\lambda) L(\lambda) d\lambda$$

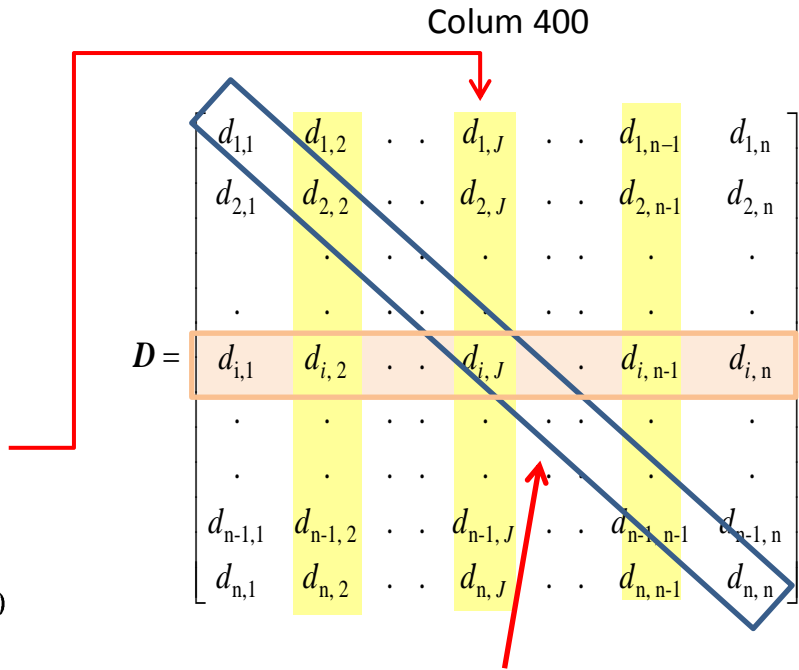


$$S_{meas} = S_{IB} + S_{SL}$$

$S_{Stray\ Light}$: Development of the SDF Matrix



The SDF matrix, $D_{n \times n}$



Zero's along the diagonal



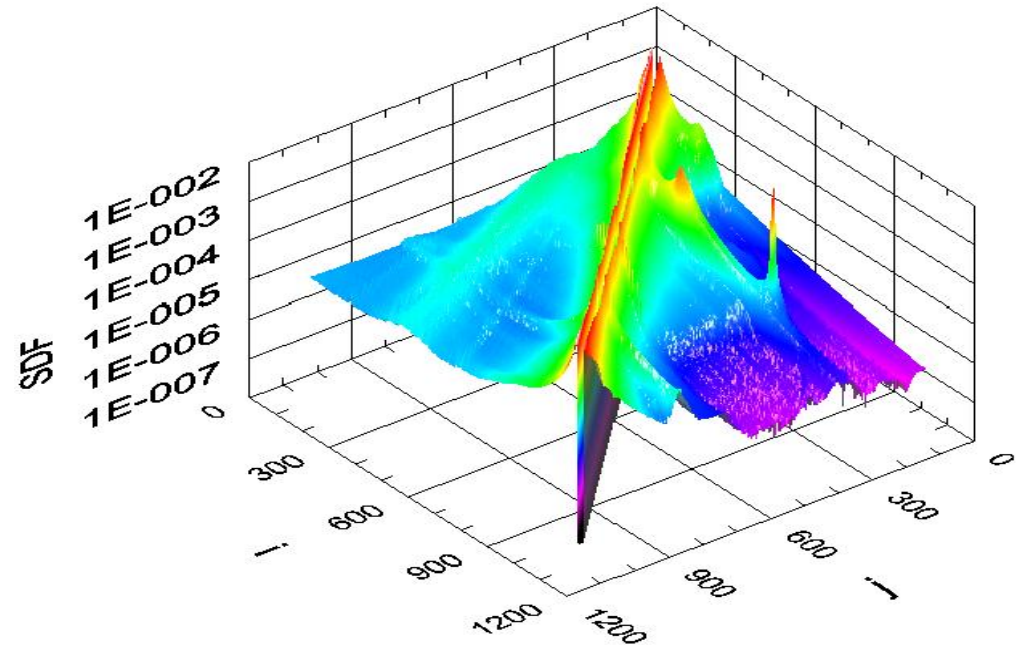
Relative scattering from pixel j into all other pixels in the array



Relative scattering from all other pixels in the array into pixel i

The Stray Light Distribution (SDF) matrix, \mathbf{D}

$$\mathbf{D} = \begin{bmatrix}
 d_{1,1} & d_{1,2} & \cdot & \cdot & d_{1,J} & \cdot & \cdot & d_{1,n-1} & d_{1,n} \\
 d_{2,1} & d_{2,2} & \cdot & \cdot & d_{2,J} & \cdot & \cdot & d_{2,n-1} & d_{2,n} \\
 \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\
 d_{i,1} & d_{i,2} & \cdot & \cdot & d_{i,J} & \cdot & \cdot & d_{i,n-1} & d_{i,n} \\
 \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\
 \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\
 d_{n-1,1} & d_{n-1,2} & \cdot & \cdot & d_{n-1,J} & \cdot & \cdot & d_{n-1,n-1} & d_{n-1,n} \\
 d_{n,1} & d_{n,2} & \cdot & \cdot & d_{n,J} & \cdot & \cdot & d_{n,n-1} & d_{n,n}
 \end{bmatrix}$$



A little Matrix Algebra ...

$$S_{SL} = \vec{D} \square S_{IB}$$

$$S_{meas} = S_{IB} + \vec{D} \square S_{IB}$$

$$S_{meas} = [I + \vec{D}] \square S_{IB}$$

$$S_{IB} = [I + \vec{D}]^{-1} \square S_{meas}$$

$$C = [I + \vec{D}]^{-1}$$

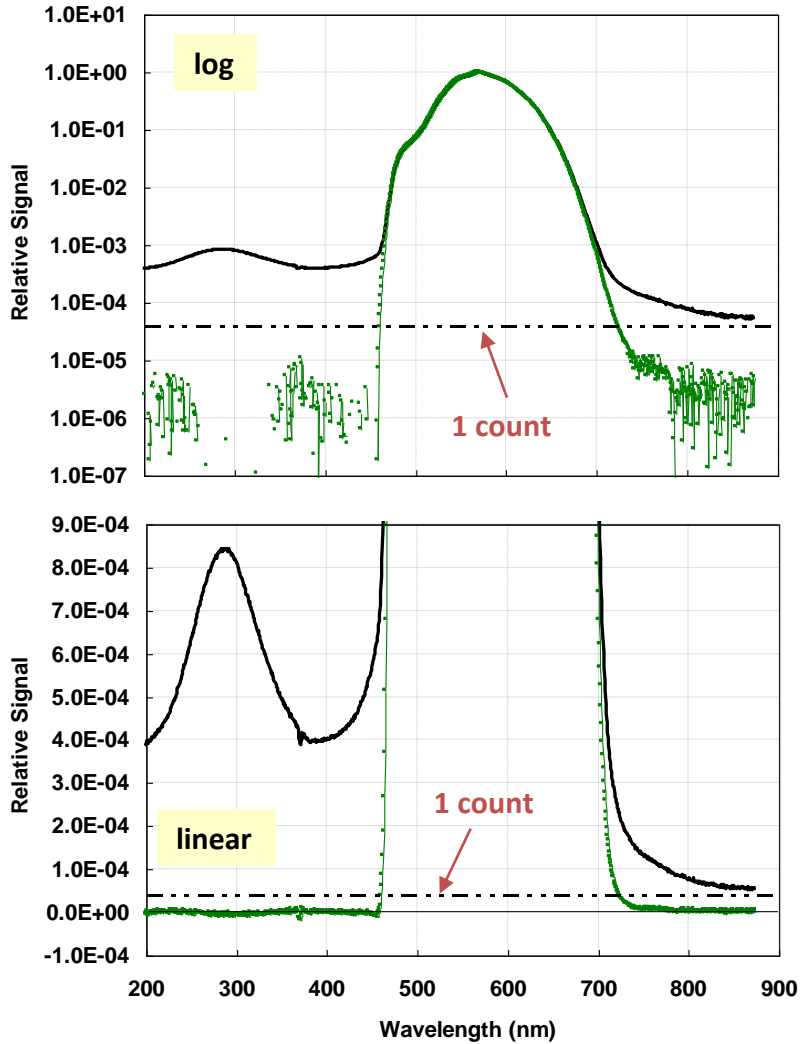
$$S_{IB} = C \square S_{meas}$$

“Truth”

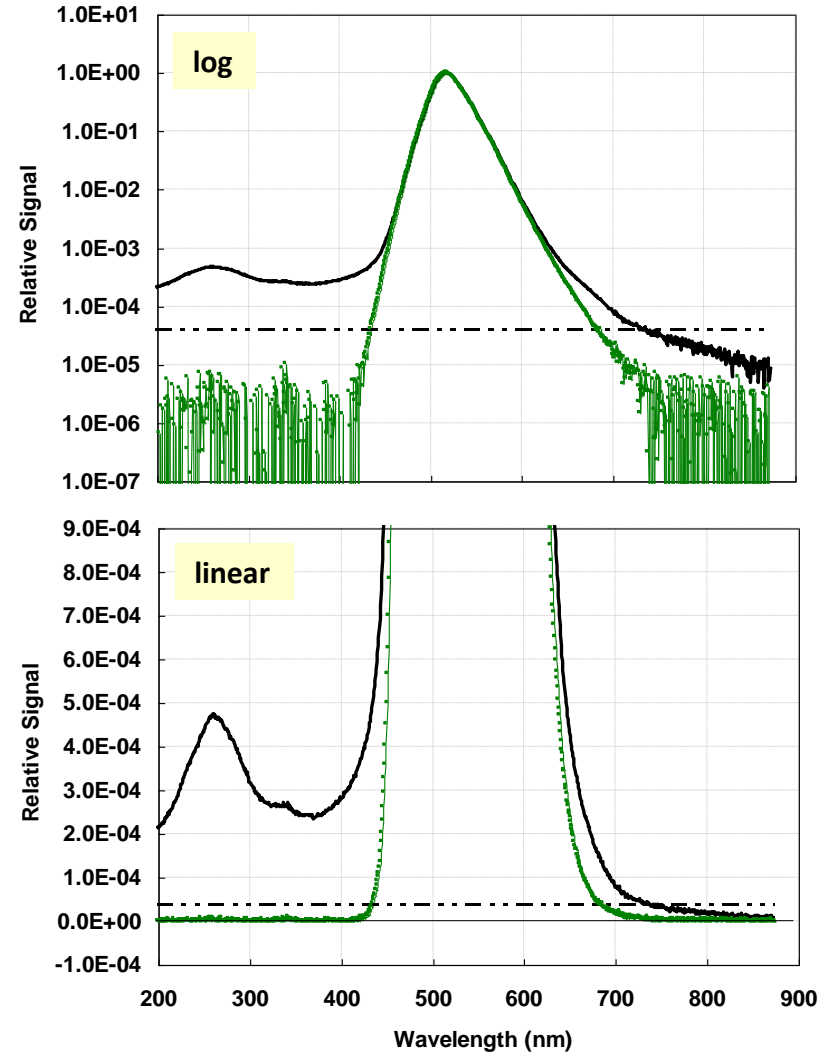
**Stray-light
correction matrix.**

Two Example Results of Stray-light Correction

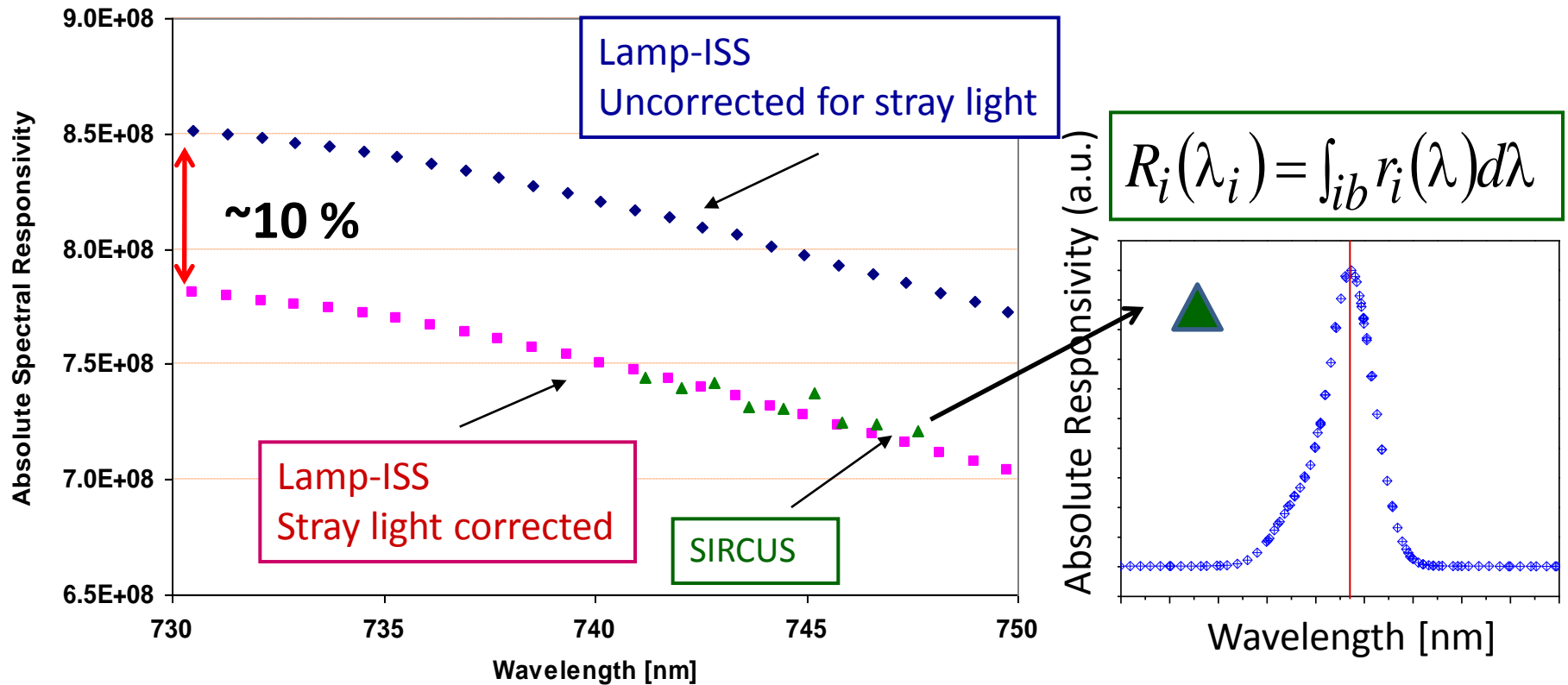
A Green Optical Filter



A Green LED



Magnitude of Stray Light: Broadband v. Narrowband calibrations



Extension of the Algorithm to a Multiple Channel Spectrograph

- Take each of the input channels and create one long $n \times 1$ matrix, where $n = \#$ of channels multiplied by the number of elements in the array (dispersion direction)
- Example:
 - For a system with 4 inputs, 1024 elements in the along track direction, the array is a 4096×1 array

As with the 1-d case,

$$S_{SL} = \vec{D} \square S_{IB}$$

Only D and S now have different meanings.

Consider a 4-channel system

$$\vec{D} \square S_{IB} = \begin{bmatrix} \vec{D}_{11} & \vec{D}_{12} & \vec{D}_{13} & \vec{D}_{14} \\ \vec{D}_{21} & \vec{D}_{22} & \vec{D}_{23} & \vec{D}_{24} \\ \vec{D}_{31} & \vec{D}_{32} & \vec{D}_{33} & \vec{D}_{34} \\ \vec{D}_{41} & \vec{D}_{42} & \vec{D}_{43} & \vec{D}_{44} \end{bmatrix} \begin{bmatrix} S_{IB}^1 \\ S_{IB}^2 \\ S_{IB}^3 \\ S_{IB}^4 \end{bmatrix}$$

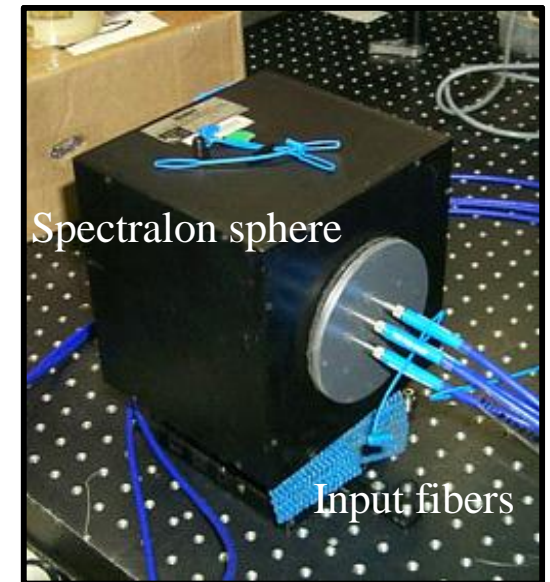
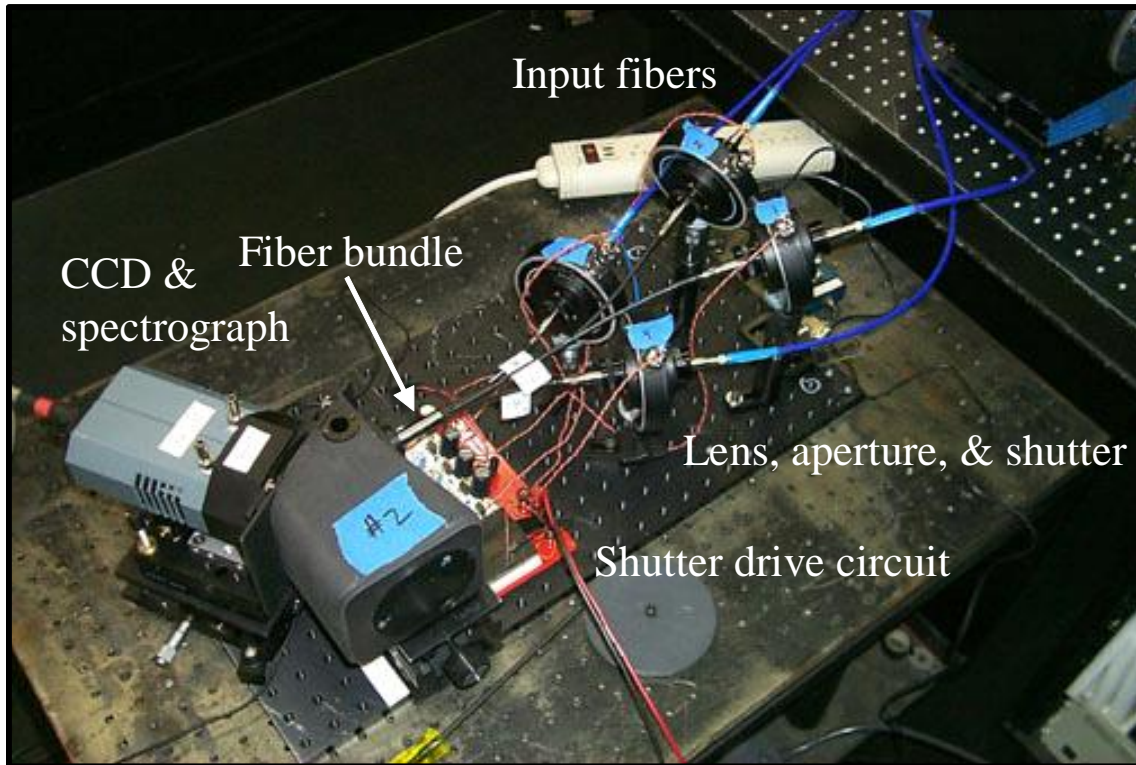
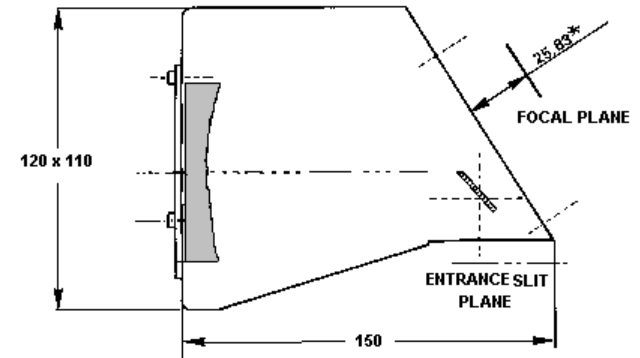
\vec{D} matrix now comprised of sub-arrays

$\vec{D}_{i,i}$ describes the along-track scattering

$\vec{D}_{i,j}$ describes the cross-track scattering from track I into track j

Multiple Input Spectrograph System

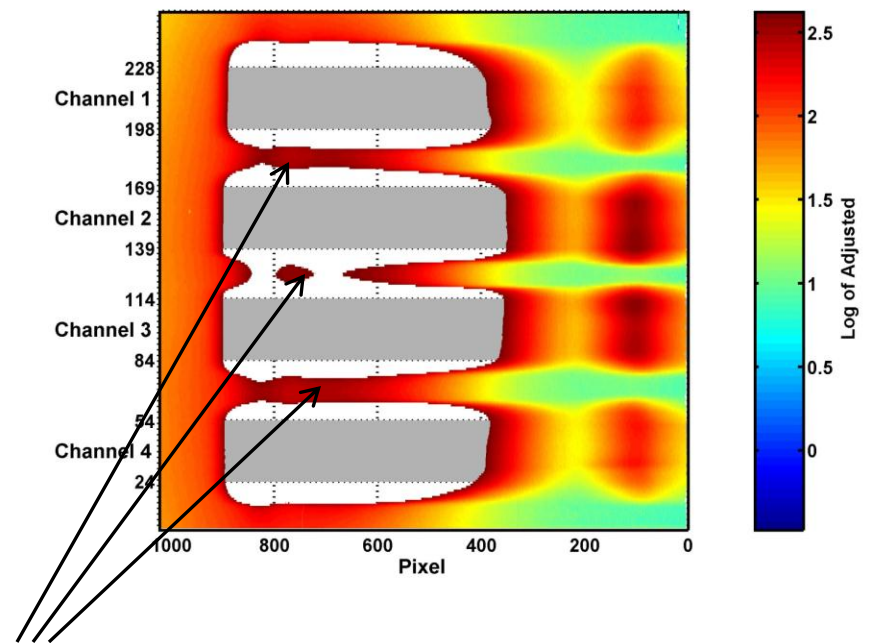
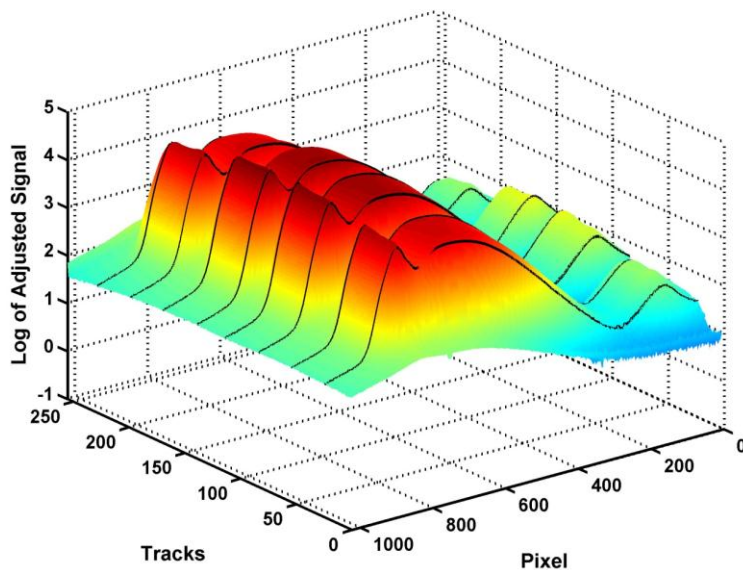
- ISA (Jobin Yvon) f/2 spectrograph with reflective concave holographic grating; 25 mm slit
- Andor 1024x256 cooled CCD array, 25 mm pixels
- Breadboard system had 4 1 mm fibers separated by ~500 mm



4-Channel Input into Spectrograph

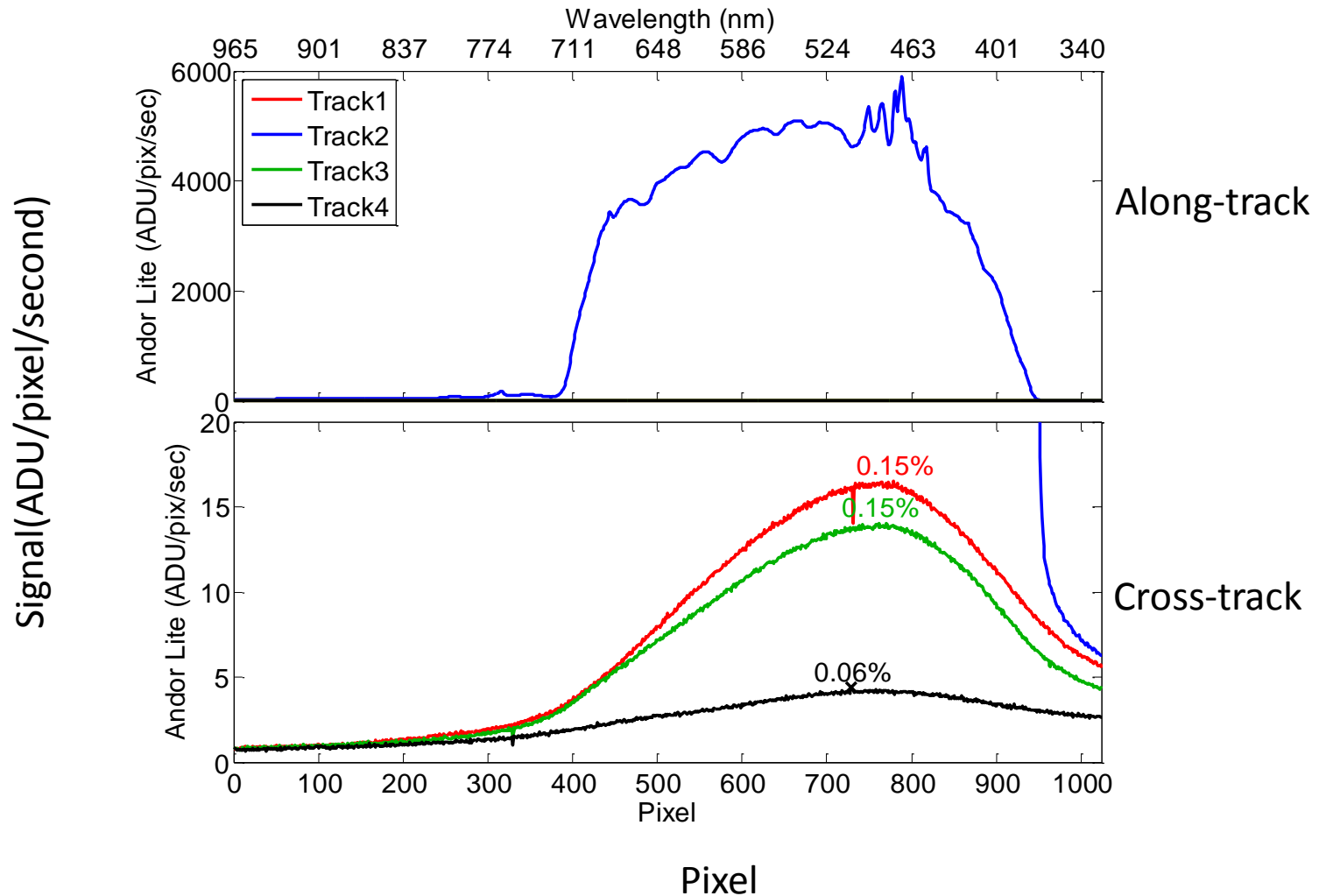
All 4 channels illuminated with LED

Image expanded to 1 % full scale

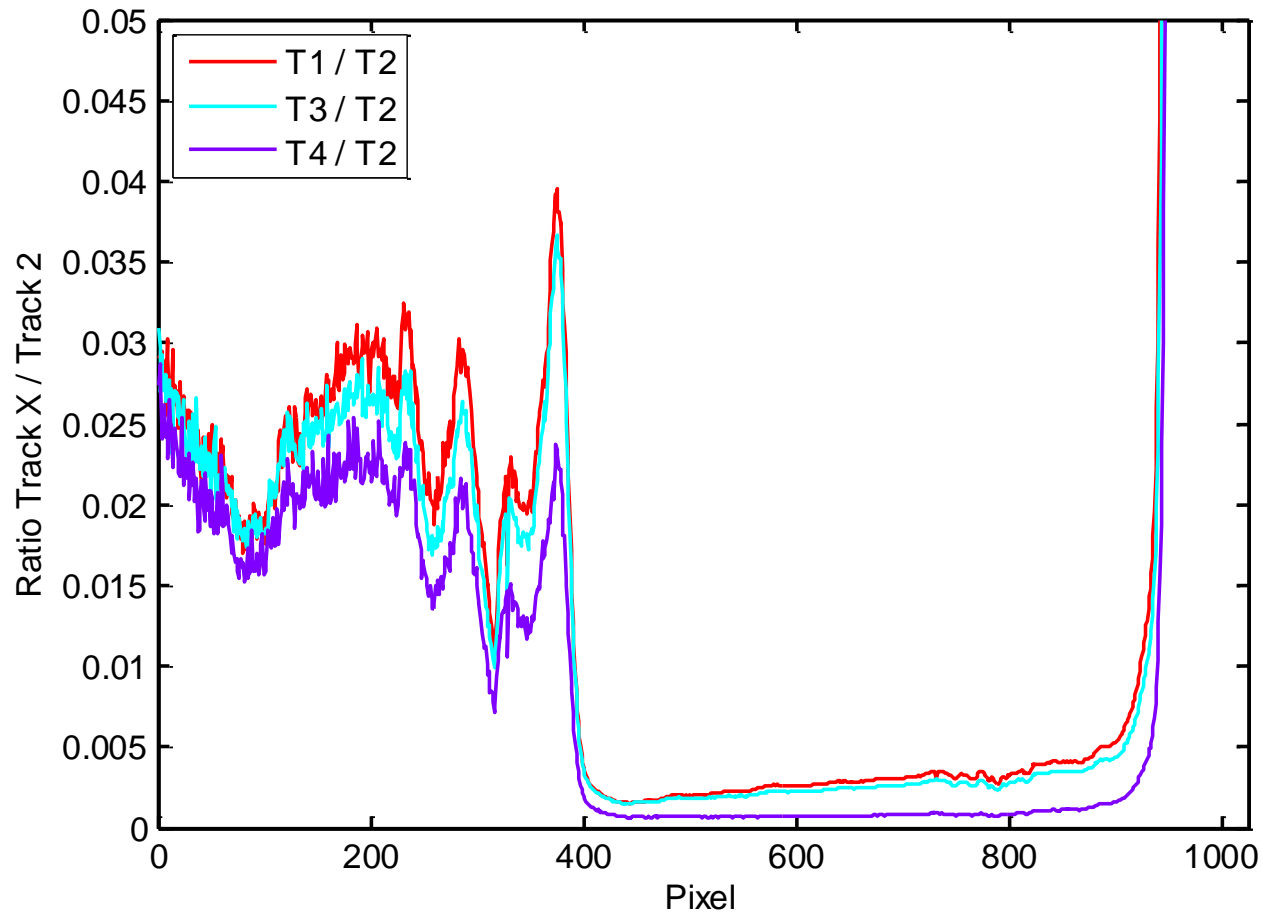


Cross-track coupling

Xenon source, Only Track 2 Illuminated

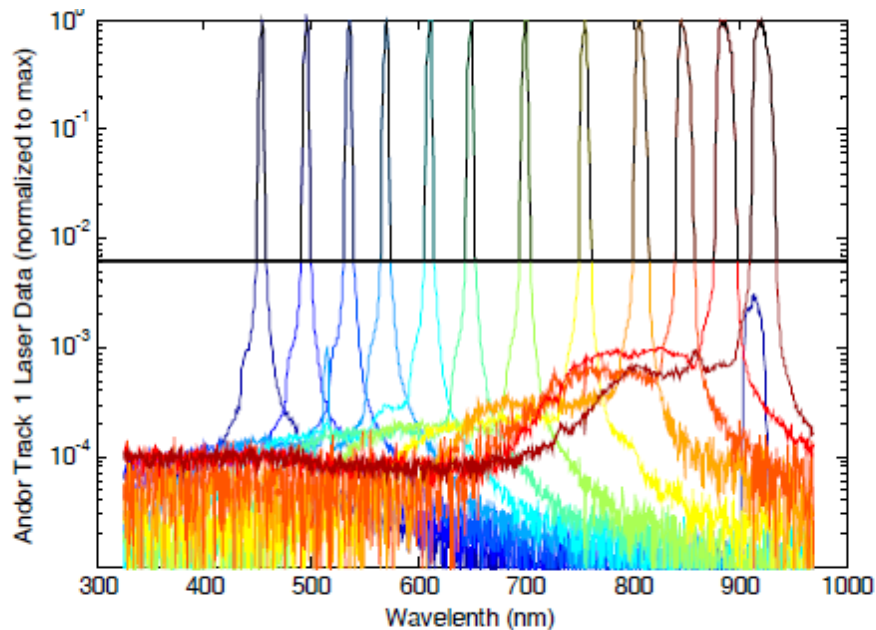


Ratio of Track x to Track 2

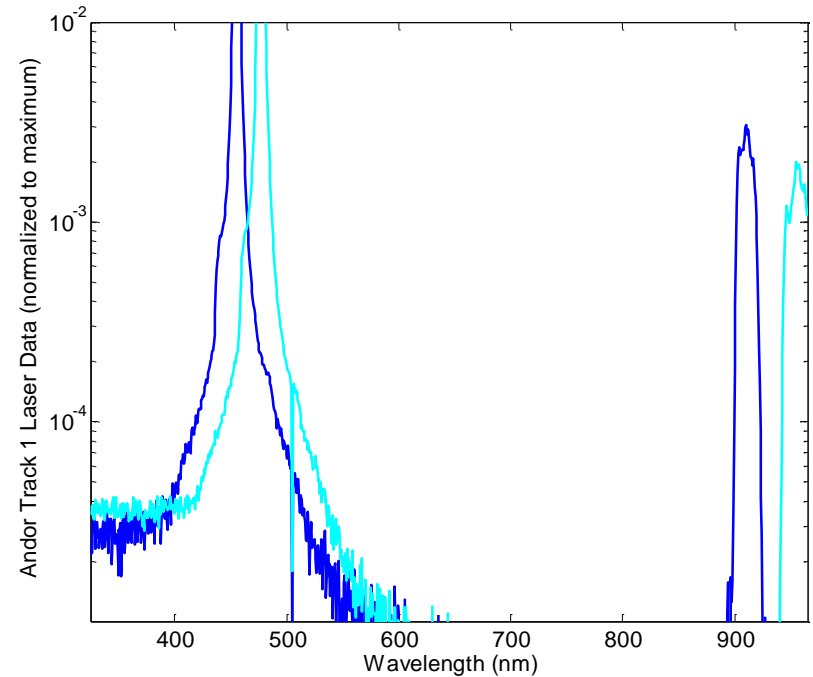


Stray light characterization using tunable lasers

Laser characterization data (subset of full data set)



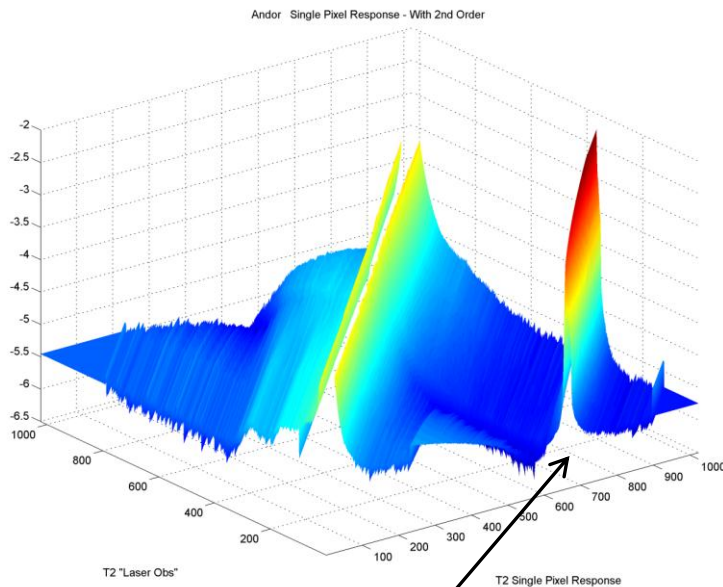
Second order diffraction



Stray Light Distribution Function Matrix

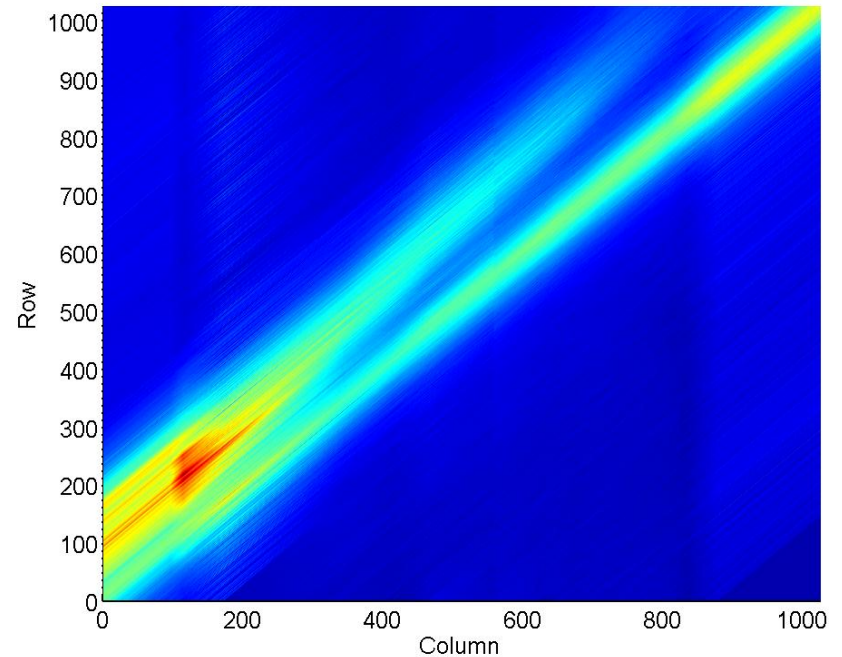
(normalized by the in-band area)

Along-track Sub-Matrix D_{22}



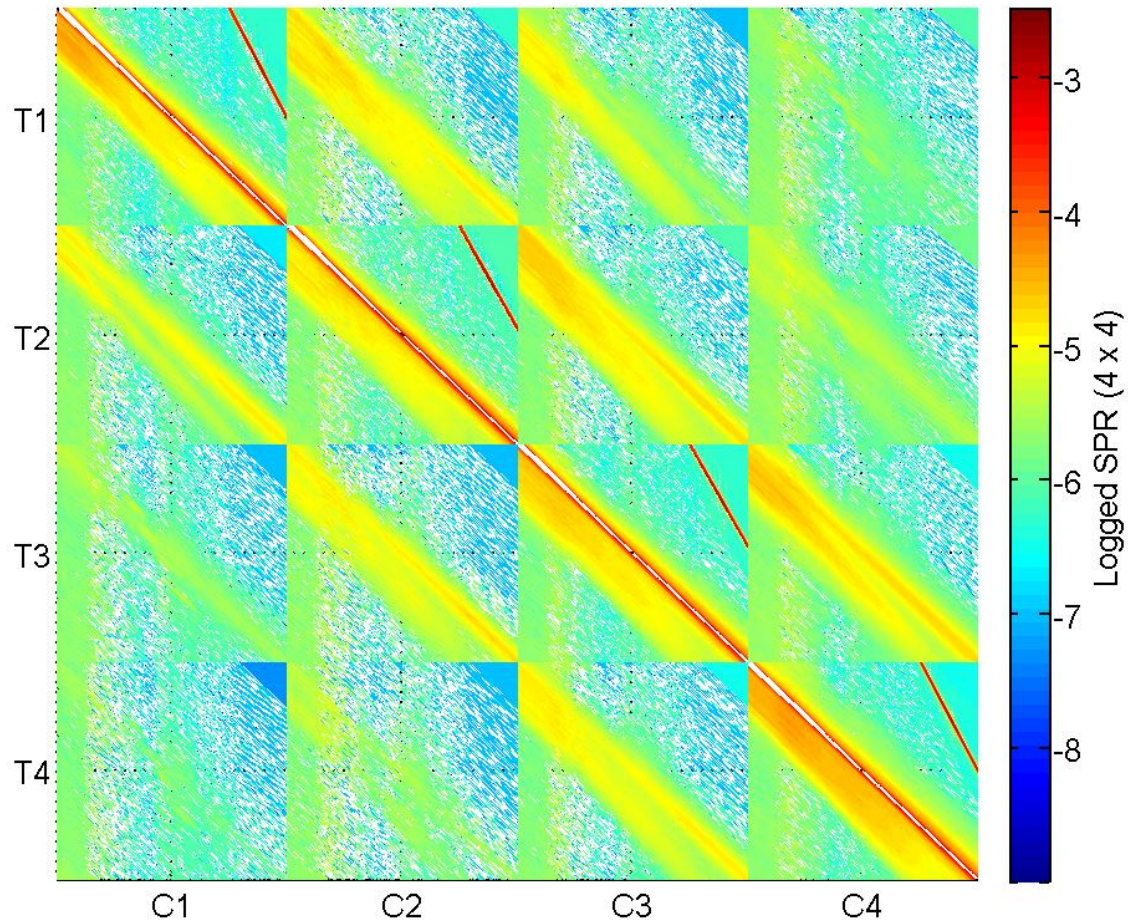
Second order diffraction peak

Cross-track Sub-Matrix D_{43}

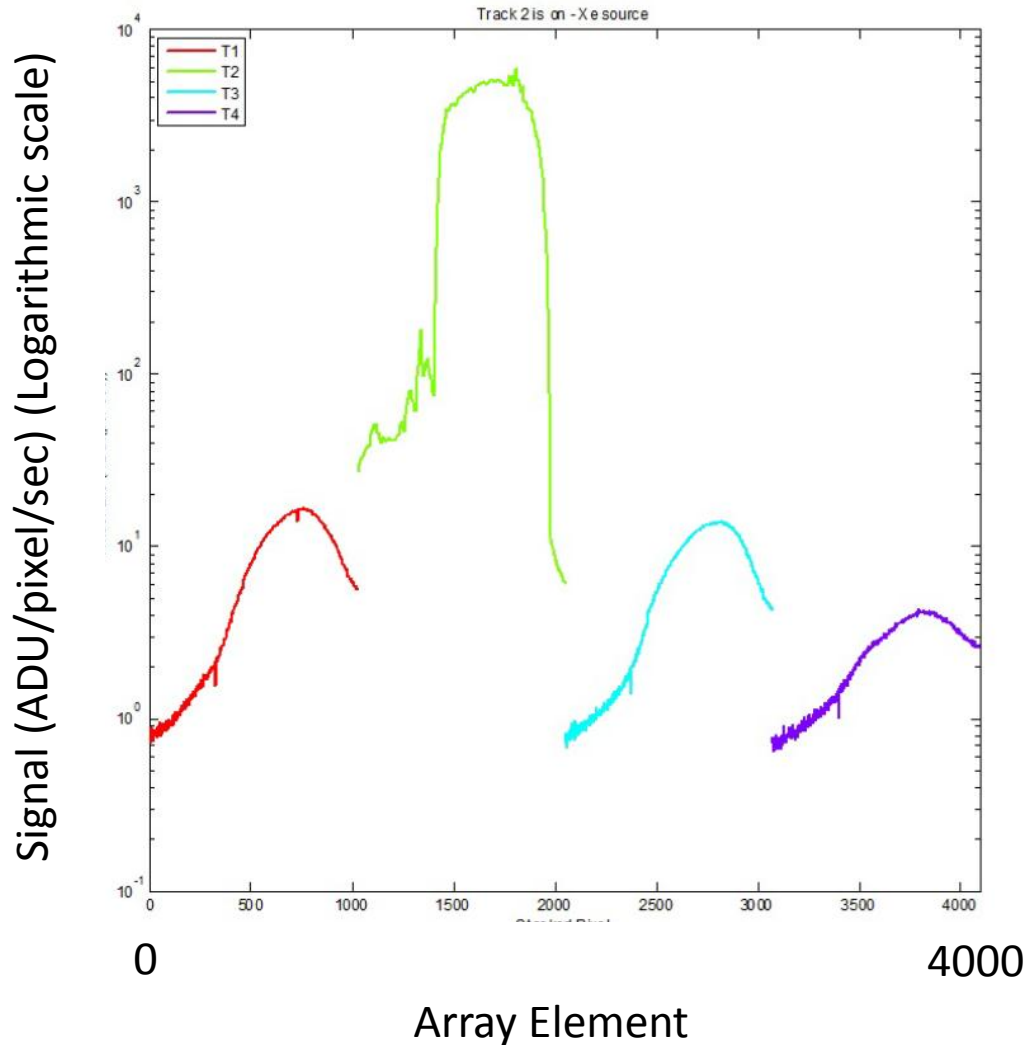


Not zero along the diagonal

4-channel D-matrix



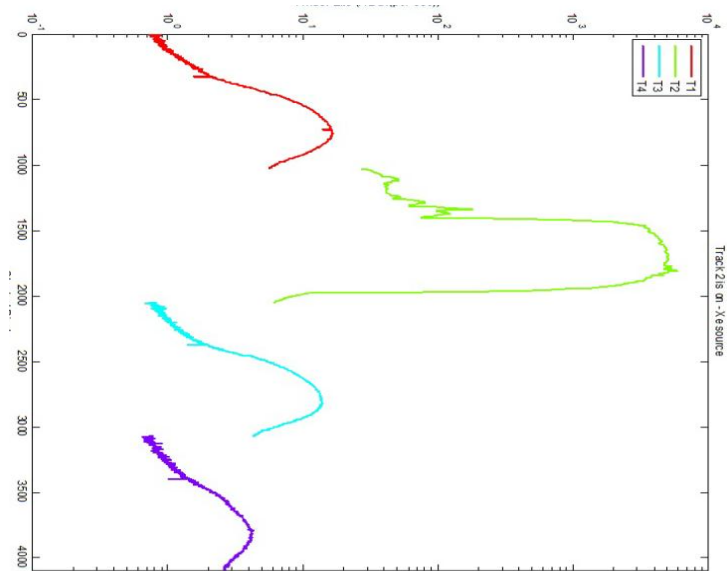
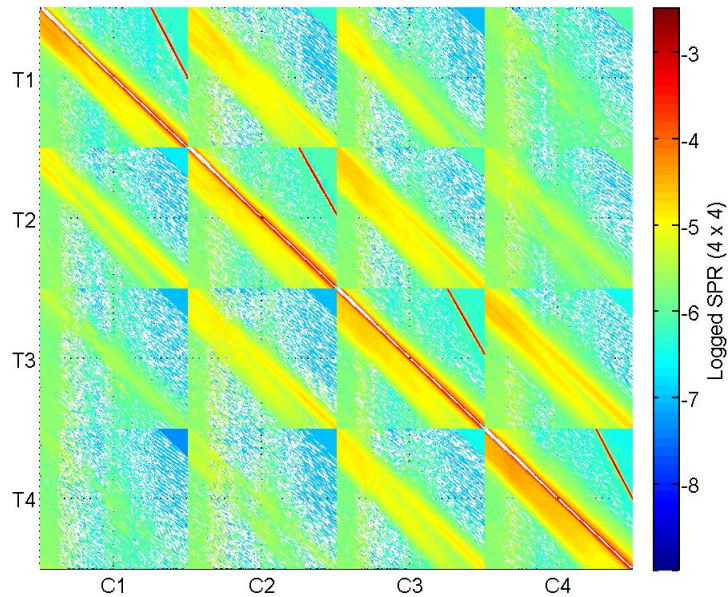
S_{meas} : Track 2 only Illuminated



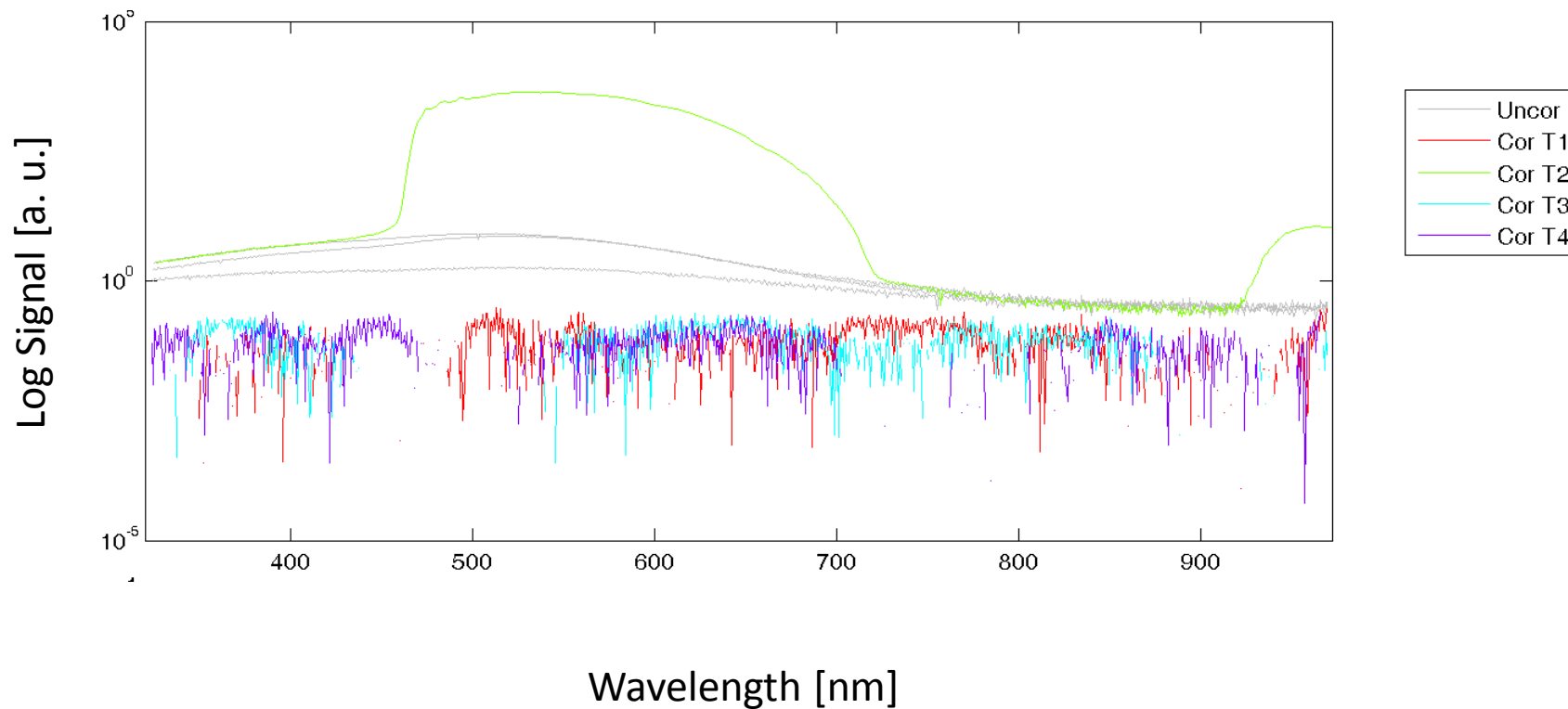
$$\vec{D} \square S_{IB} = \begin{bmatrix} \vec{D}_{11} & \vec{D}_{12} & \vec{D}_{13} & \vec{D}_{14} \\ \vec{D}_{21} & \vec{D}_{22} & \vec{D}_{23} & \vec{D}_{24} \\ \vec{D}_{31} & \vec{D}_{32} & \vec{D}_{33} & \vec{D}_{34} \\ \vec{D}_{41} & \vec{D}_{42} & \vec{D}_{43} & \vec{D}_{44} \end{bmatrix} \begin{bmatrix} S_{IB}^1 \\ S_{IB}^2 \\ S_{IB}^3 \\ S_{IB}^4 \end{bmatrix}$$

D

S



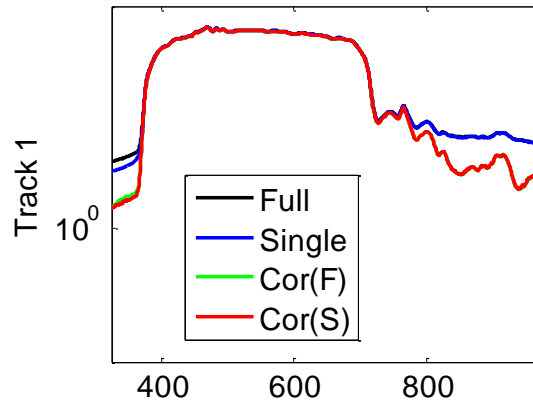
Validation: Single track Illuminated



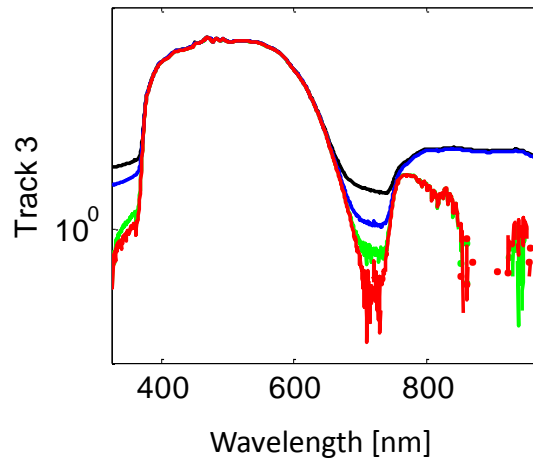
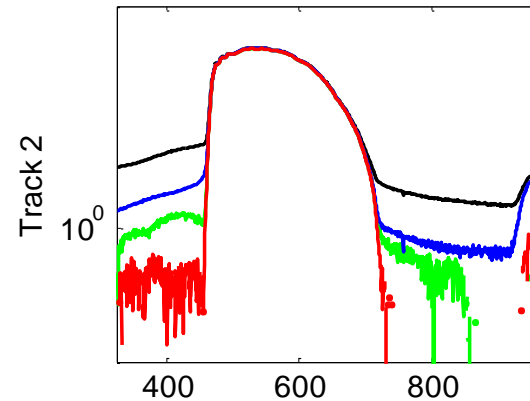
Validation (Logarithmic Scale)

Full = all tracks illuminated; Single = single track illuminated

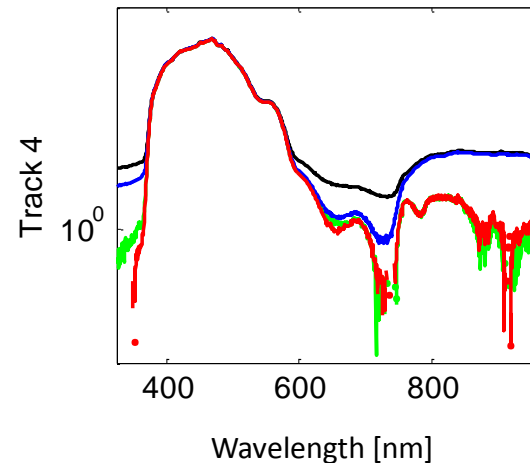
Xe source



Xe source, PER filter



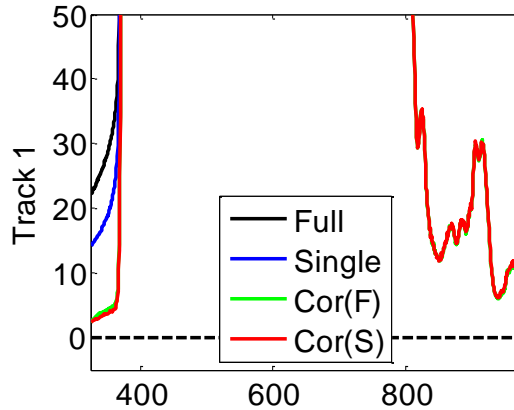
Xe source, BG-39 filter



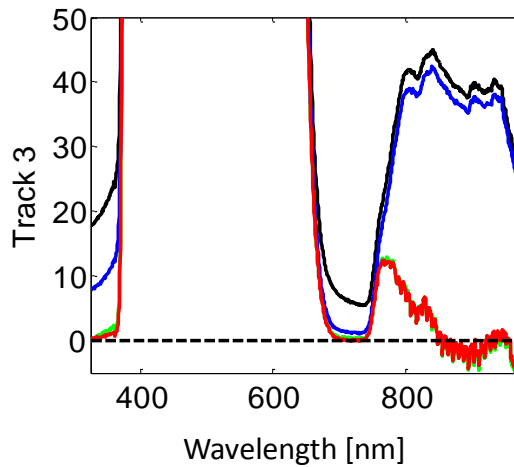
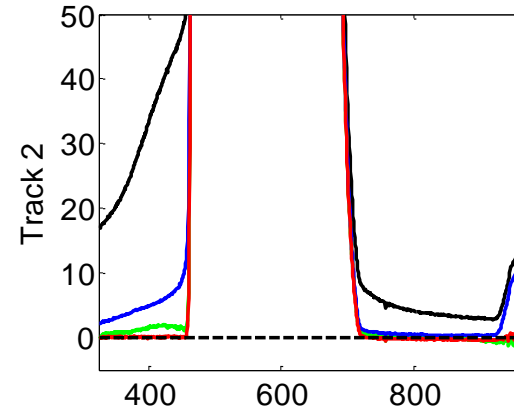
Xe source, BG-28 filter

Validation (Linear Scale)

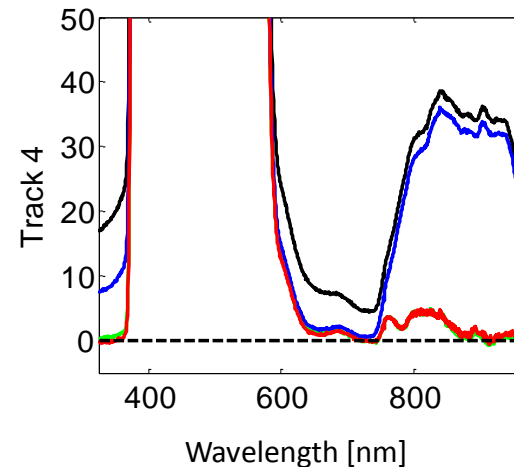
Xe source



Xe source, PER filter

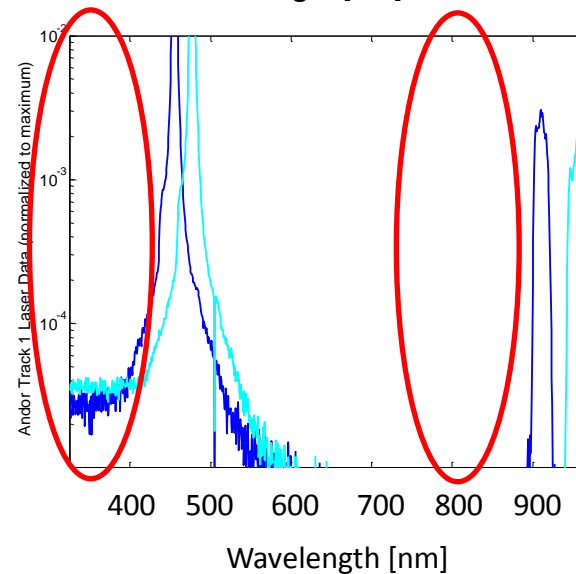
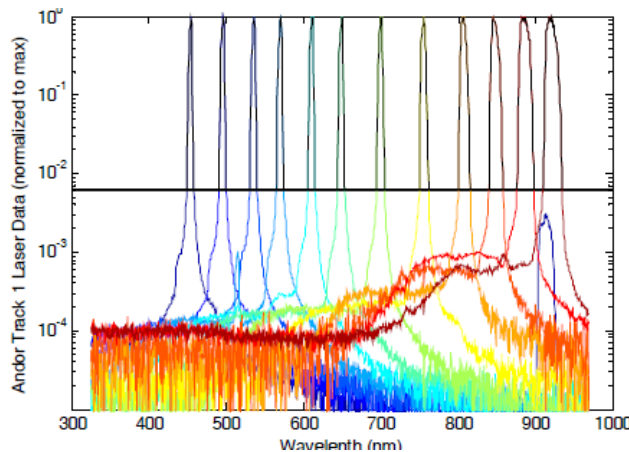
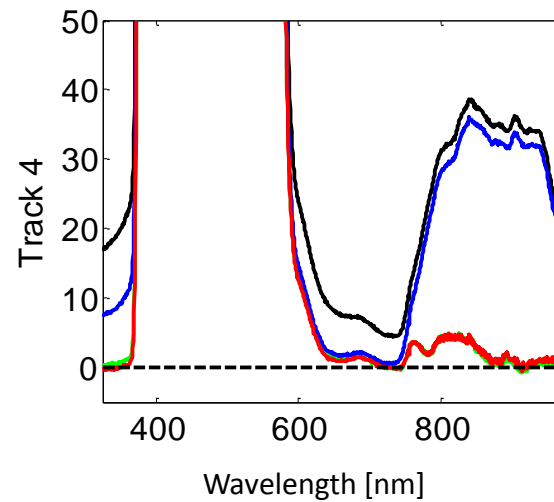
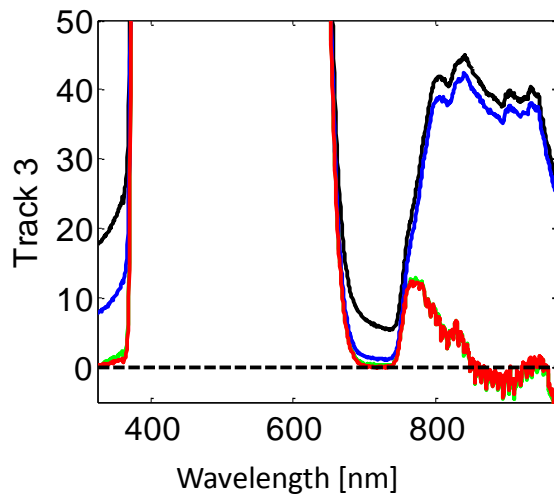


Xe source, BG-39 filter

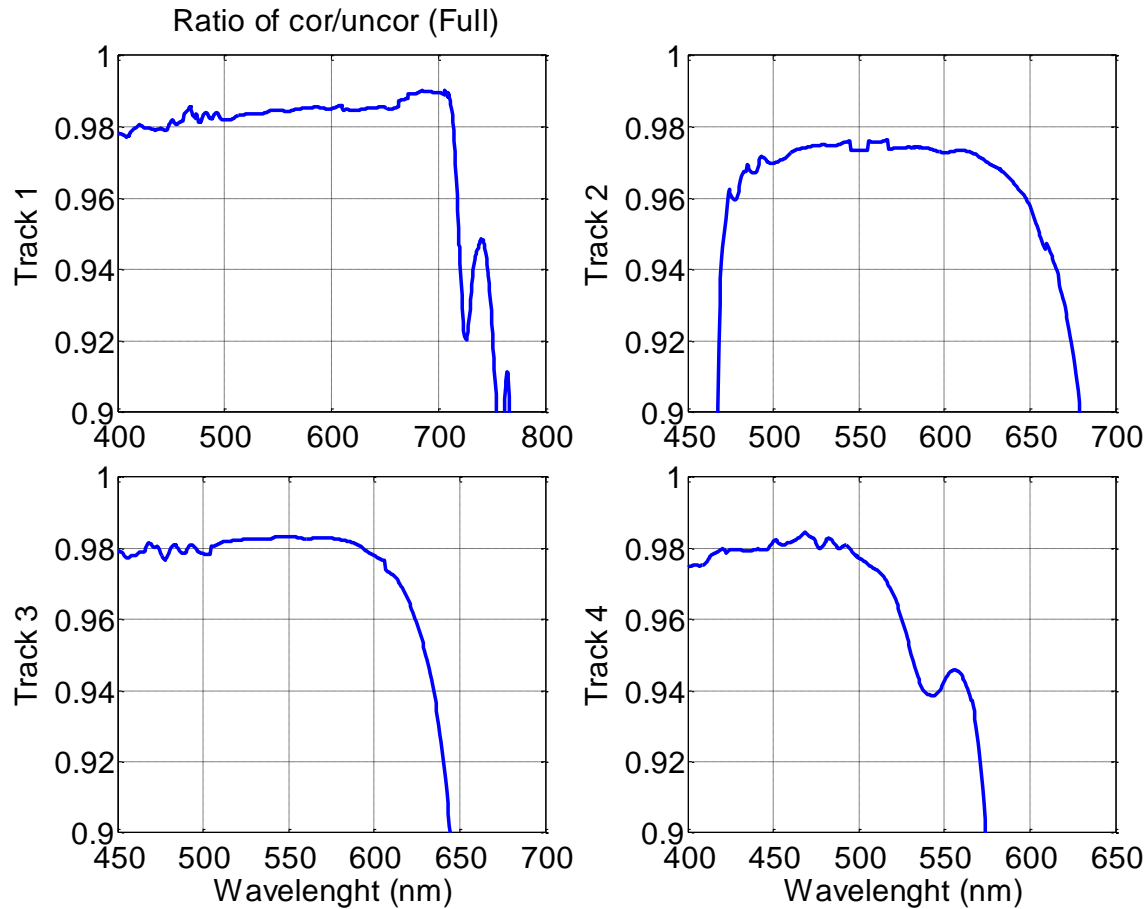


Xe source, BG-28 filter

Residual signal near 800 nm originates from incomplete characterization

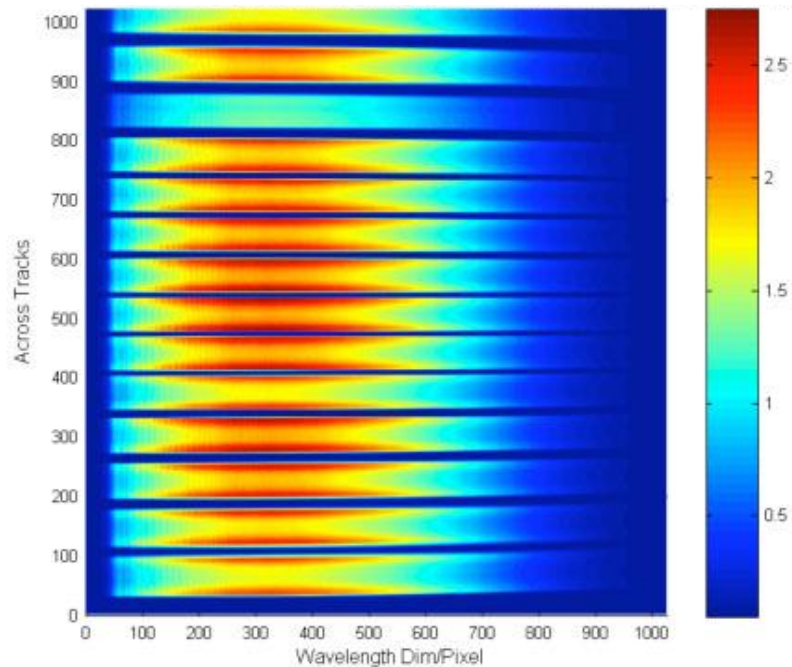


Magnitude of the correction

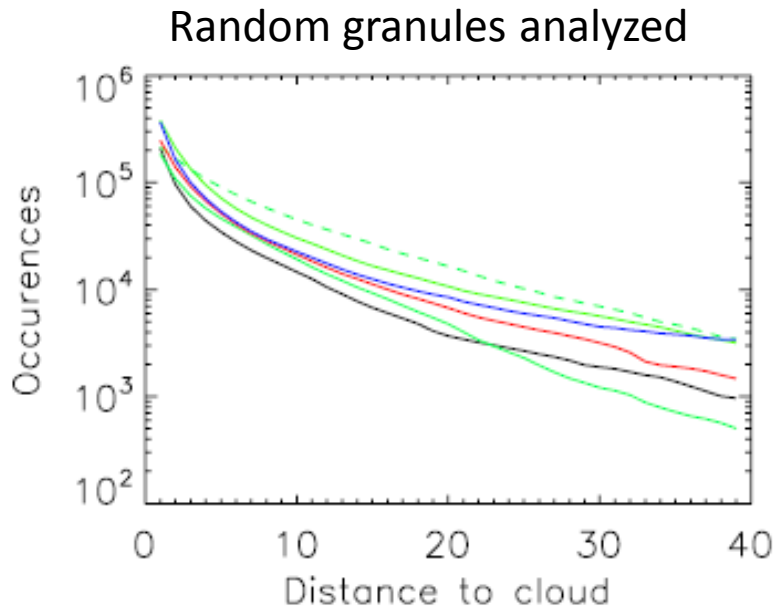


Future Direction: Finite Point Spread Response correction

- Limit as the width of a channel decreases to one pixel and the # of channels increases to # of elements



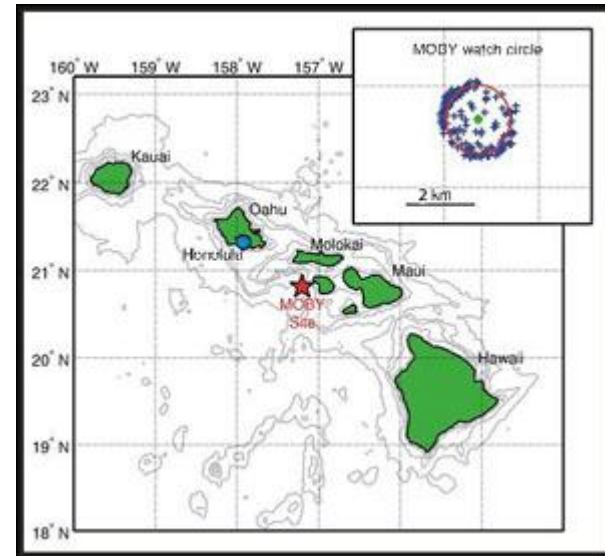
Proposed point spread response correction for MODIS



Y-axis Logarithmic scale
For these granules, most measured elements are close to clouds!

Analysis of a time series of imagery (same site, different cloud cover)

1. Ground truth site (MOBY Site)

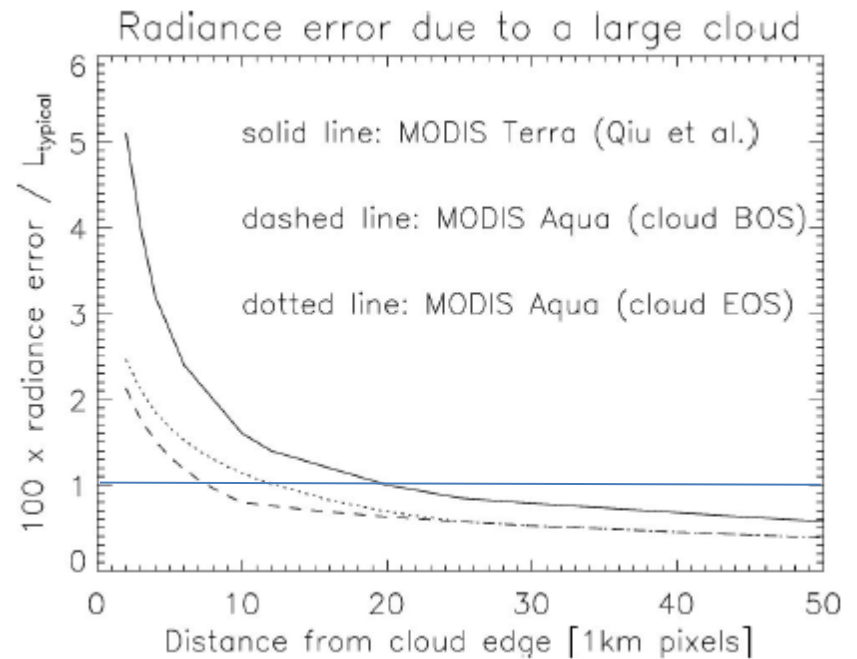
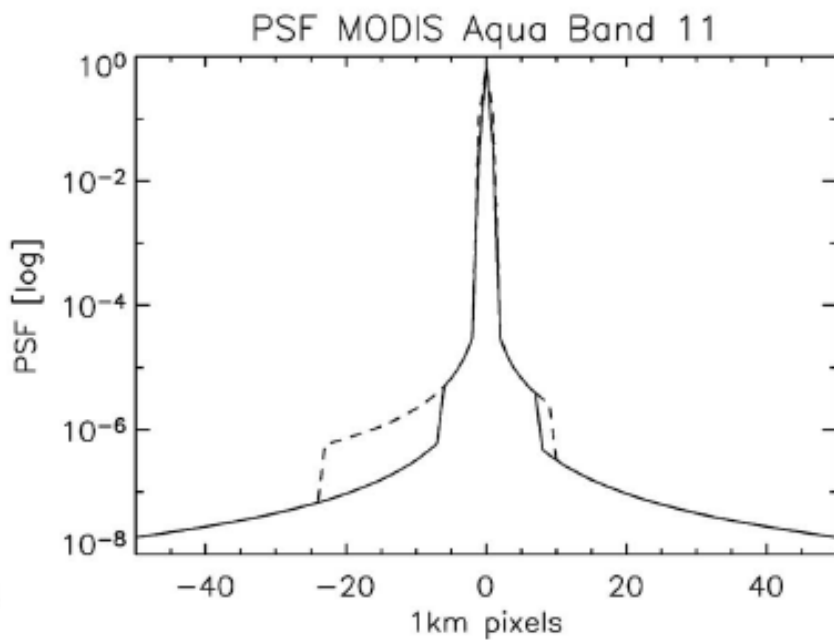


2. A site where the radiometric properties of the ocean are known and constant

Southern Ocean?

Future Direction

- MODIS



(Band 11 centered at 531 nm)

Gerhard Meister and Charles R. McClain, Appl. Opt. 49, 6276-6285 (2010)

Thank you for your attention.